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# ENVIRONMENTAL GEOLOGY NOTES

JUNE 1975 • NUMBER 75

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## DATA FROM CONTROLLED DRILLING PROGRAM IN KANE COUNTY, ILLINOIS

Philip C. Reed

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ILLINOIS STATE GEOLOGICAL SURVEY

Jack A. Simon, Chief



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# DATA FROM CONTROLLED DRILLING PROGRAM IN KANE COUNTY, ILLINOIS

*Philip C. Reed*

## ABSTRACT

Samples of earth materials were collected at eight sites in Kane County, Illinois, as part of a controlled drilling program for ground-water exploration in northeastern and north-central Illinois. Descriptions of the character and sequence, tables listing relative density, relative consistency, moisture content, and size analyses, and gamma-ray logs are presented for the glacial materials sampled and tested in the program.

## INTRODUCTION

In the Chicago region and in other areas of northern Illinois, the deep sources of water, the artesian sandstones, are already overpumped. To seek information on the nature of glacial deposits in order to facilitate the search for new, shallow sources of ground water for the rapidly expanding metropolitan areas of northeastern and north-central Illinois, the Illinois State Geological Survey has conducted controlled drilling programs. Data compiled from field and laboratory analyses of samples collected from eight drill holes in Kane County are presented here (fig. 1). The test holes were drilled in conjunction with an aquifer-evaluation study by the Illinois State Water Survey.

The Geological Survey's role in the investigation was to obtain, by controlled drilling, sampling, and testing, detailed information on the glacial deposits in the larger buried valleys in Kane County. These valleys were believed to have a reasonably good potential as a source of ground water. Previously, little test drilling had been done to determine the nature of the valley deposits and their ground-water potential.

The Illinois State Water Survey has made quantitative appraisals of the water-yielding potential of the glacial deposits at selected sites in north-eastern and north-central Illinois. In subsequent reports the Geological Survey will present geologic interpretations of the data reported here. The results of controlled drilling programs conducted in 1962-63 and in 1970 were reported in earlier Environmental Geology Notes (nos. 2, 6, 7, 9, 10, 53, and 71).

Data from controlled drilling programs can be applied to other environmental problems in northeastern and north-central Illinois in addition to the availability of ground water. These investigations (1) supplement existing information on the character and distribution of glacial materials that may be usable mineral resources, that may present construction problems, or that affect the disposal of wastes; and (2) provide a basis for interpreting other types of subsurface information, such as drillers' logs of water wells or records of foundation borings. For example, the drilling provided representative, relatively undisturbed split-spoon samples of earth materials that can be used to determine the physical and chemical properties that commonly affect land use.

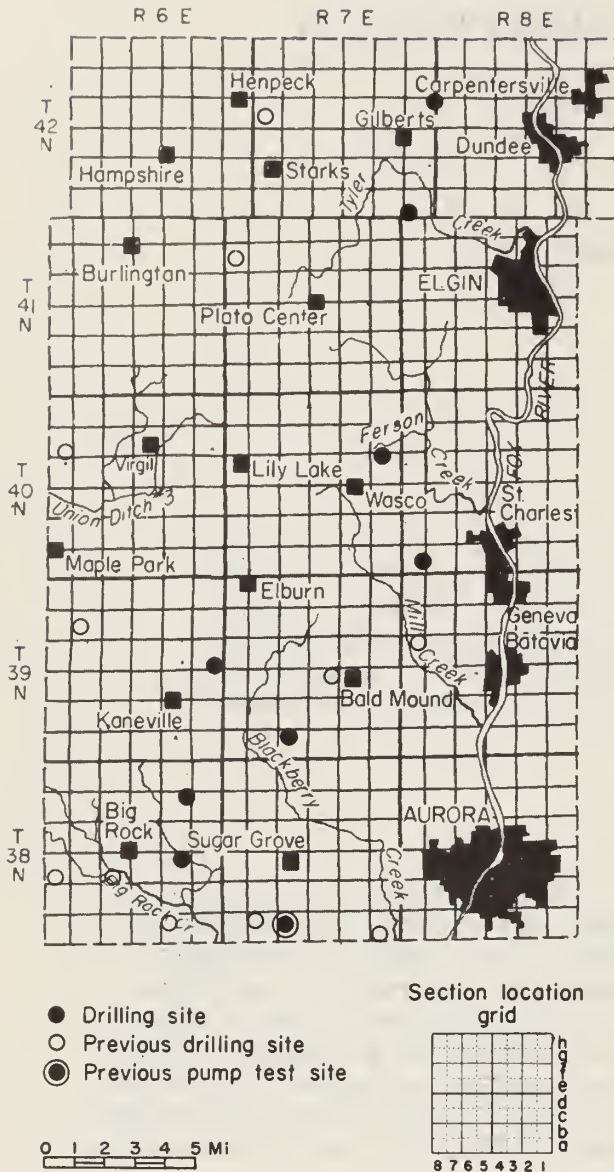


Fig. 1 - Location of drilling sites in Kane County.

The exploratory test holes were drilled by Layne-Western Company of Aurora, Illinois, under the supervision of the Geological Survey. Locations for the test holes selected by the Geological Survey were generally along the rights-of-way of county roads. Landowners and utility companies were consulted about buried tiles, cables, and pipelines in the area. County and township road supervisors, county zoning and planning officials, and county health officers were apprised of the scope, progress, and results of the testing.



## FIELD OPERATIONS

### Drilling

The drilling contractor was provided with a log of the anticipated thickness and character of the deposits extending to bedrock, instructions on testing procedures, and a list of depths to be sampled with a split-spoon sampler. A mobile Sanderson-Cyclone hydraulic rotary drill rig was used for the drilling. The support equipment consisted of an 18-foot tilt trailer, a 1,000-gallon flat-bedded water truck, an enclosed 12-foot test site trailer, and a 1½-ton truck with a rear mounted backhole. The crew at the rig normally was made up of a driller, a driller's helper, and a Survey geologist. During drilling, conventional rotary samples were obtained, split-spoon samples were taken at selected intervals, and a log was made of the materials penetrated.

Interconnected settling and suction pits of about equal size were used during the program to keep the drilling mud at optimum viscosity and weight. The mud losses during drilling and between work periods were recorded for each boring. Natural mud alone was used to start test holes, but eventually bentonite and, periodically, caustic soda were added to improve mud properties. Density and viscosity of the drilling mud were determined with a standard mud balance and a Marsh funnel.

### Sampling

Rotary samples were collected at 5-foot intervals from the open ditch near the drill hole. The drilling mud was circulated until a representative sample was collected from each interval. The samples were washed in a 5-gallon bucket, air dried, and then bagged.

Split-spoon samples were obtained with a sampler having an outside diameter (OD) of 2 inches. The split-spoon was lowered inside a full-hole 4½-inch OD drill pipe on AW-Rod (OD 1¾ inches) with flush-joint straight thread. The spoon was then driven 18 inches by a 140-pound hammer that fell 30 inches or, where noted, by a 300-pound stem and jar that fell 27 inches. The rotary cuttings and the split-spoon samples are on file at the Geological Survey.

Measurements of the unconfined compressive strength of cohesive materials (primarily clay till) were made on each split-spoon sample with a Soiltest Model CL-700 pocket penetrometer immediately after the sample was obtained. A small portion of each cohesive sample was sealed in a bottle for determination of natural moisture content.

The relations between descriptive terms and quantitative expressions for relative density and relative consistency are as follows:

| Relative density       |          | Relative consistency |                                |
|------------------------|----------|----------------------|--------------------------------|
| Description            | Blows/ft | Description          | Qp*<br>(tons/ft <sup>2</sup> ) |
| Very loose . . . . .   | 0 - 5    | Very soft . . . . .  | 0.0 - 0.25                     |
| Loose . . . . .        | 5 - 10   | Soft . . . . .       | 0.25 - 0.5                     |
| Medium dense . . . . . | 10 - 30  | Medium . . . . .     | 0.5 - 1.0                      |
| Dense . . . . .        | 30 - 50  | Stiff . . . . .      | 1.0 - 2.0                      |
| Very dense . . . . .   | 50+      | Very stiff . . . . . | 2.0 - 4.0                      |
|                        |          | Hard. . . . .        | 4.0+                           |

\* Unconfined compressive strength measurement made with pocket penetrometer.

## ELECTRIC LOGGING AND NATURAL GAMMA LOGGING

Spontaneous potential (SP), single-point resistivity, and natural gamma logs were run in mud-filled test holes with a Neltronic logger (IK Model D). The logs, which are on file at the Geological Survey, were useful in the interpretation of the lithologic sequence, character, and thickness of the glacial deposits sampled and tested in the program. The natural gamma logs are shown for each site tested.

## LABORATORY TESTS

### Size-Distribution Analyses

Hydrometer analyses were used to determine the amount of clay (particle diameter less than 0.0039 mm) in each cohesive split-spoon sample. Samples of approximately 55 grams were taken, and corrections for temperature and added deflocculants were made. The amount of material coarser than silt (diameter greater than 0.0625 mm) was determined by sieving, and the amount of silt was determined by subtracting from the weight of the total sample the weight of the coarser material plus the weight of clay.

The rotary and split-spoon samples that were friable and noncohesive were sieved with Tyler screens. The dimensions of the sieves and the Wentworth and phi ( $\phi$ ) grain-size classifications related to this study are shown in table 1. The upper size limit of the sieved material was about 30 mm in diameter.

TABLE 1—SIEVE DIMENSIONS AND GRADE SCALES

| Sieve number          |       | Tyler mesh diameter |        | Wentworth grain-size classification    | Phi ( $\phi$ ) scale |
|-----------------------|-------|---------------------|--------|--|----------------------|
| U.S. Standard         | Tyler | (in.)               | (mm)   |  |                      |
| 4                     | 4     | 0.1874              | 4.76   | Granules and pebbles (gravel)          |                      |
| 10                    | 9     | 0.0787              | 2.00   | ----- 2.0 mm -----<br>Very coarse sand | -1.0                 |
| 18                    | 16    | 0.0394              | 1.00   | ----- 1.00 mm -----                    | 0.0                  |
| 25                    | 24    | 0.0278              | 0.707  | Coarse sand                            |                      |
| 35                    | 32    | 0.0197              | 0.500  | ----- 0.500 mm -----                   | 1.0                  |
| 45                    | 42    | 0.0139              | 0.354  | Medium sand                            |                      |
| 60                    | 60    | 0.0098              | 0.250  | ----- 0.250 mm -----                   | 2.0                  |
| 80                    | 80    | 0.0070              | 0.177  | Fine sand                              |                      |
| 120                   | 115   | 0.0049              | 0.125  | ----- 0.125 mm -----                   | 3.0                  |
| 170                   | 170   | 0.0035              | 0.088  | Very fine sand                         |                      |
| 230                   | 250   | 0.0025              | 0.0625 | ----- 0.0625 mm -----<br>Silt          | 4.0                  |
| Hydrometer separation |       |                     |        | ----- 0.0039 mm -----<br>Clay          | 8.0                  |

#### IDENTIFICATION SYSTEM

The numbering system used to identify the borings is based on the location of the boring. The number of each hole consists of a county abbreviation and the numbers of the township, range, section, and coordinates within the section. Sections are divided into rows of one-eighth mile squares. Each square contains 10 acres and corresponds to a quarter of a quarter of a quarter section. A normal section of 1 square mile contains eight rows of one-eighth mile squares, and an odd-sized section contains more or fewer rows. Rows are numbered from east to west and lettered from south to north as shown in the grid on figure 1. For example, a well located in square 1h of Section 13, Township 42 North, Range 7 East, would be numbered KNE 42N7E-13.1h.

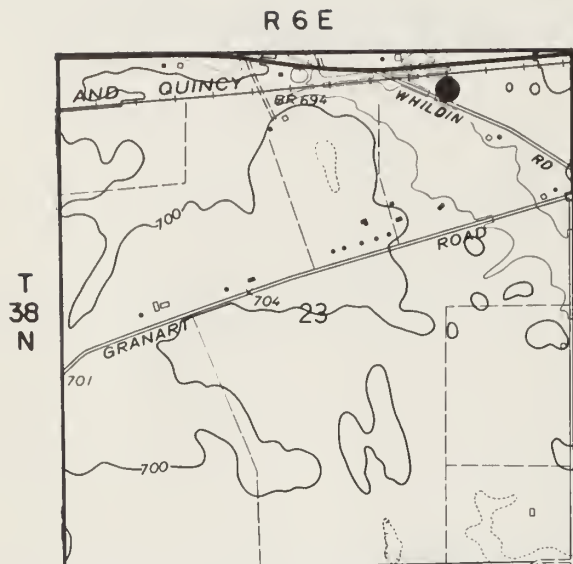
Location maps for each of the eight borings were duplicated from United States Geological Survey 7.5-minute quadrangle topographic maps (scale 1:24,000, approximately 2½ inches per mile). The borings have been located within the 10-acre coordinate squares with as much accuracy as the scales permit.

The quadrangle topographic map on which the boring is located is identified in the drill record. Elevations for each boring were estimated from contours shown on the topographic maps. Individual quadrangle maps may be purchased from the Illinois State Geological Survey, Urbana, or from the United States Geological Survey, Washington, DC.

## DATA FROM THE DRILL HOLES



DRILLING RECORD FOR KNE 38N6E-23.3h



Location of test:

S 500 ft, W 1,450 ft from NE  
cor. of sec. 23; 200 ft SE  
from a concrete culvert and  
30 ft NE of the center line  
of Whildin Road (Big Rock  
Quadrangle, 1968)

Surface elevation: 685 ft  
Date started: 7-5-72  
Date completed: 7-7-72  
Electric log interval: 0-128.0 ft  
Natural gamma log interval: 0-128.0 ft

Zones of fluid loss:

38.5-46.0  
Density: 9.5 lb/gal  
Viscosity: 39 sec/qt  
Loss: 105 gal  
47.0-60.0  
Density: 9.5  
Viscosity: 39 sec/qt  
Loss: 165 gal  
60.0-100.0  
Density: 9.9 lb/gal  
Viscosity: 44 sec/qt  
Loss: 210 gal  
100.0-120.0  
Density: 9.9 lb/gal  
Viscosity: 44 sec/qt  
Loss: 75 gal

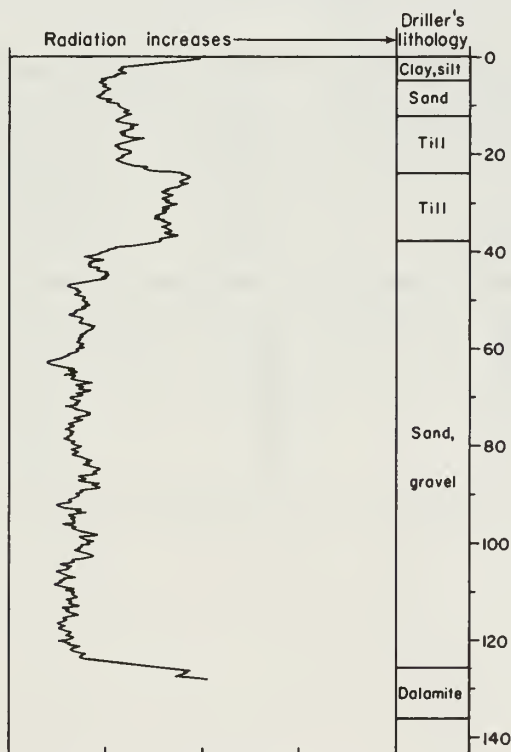
Remarks: Flow of 50 gpm (gallons  
per minute) developed overnight  
from the mud-filled borehole  
128.0 ft. deep.

KNE 38N6E-23.3h - Continued

DESCRIPTION OF MATERIALS

| Description   | Thickness<br>(ft) | Depth<br>(ft) |
|---|-------------------|---------------|
| Topsoil, black . . . . .  | 1.5               | 0.0 - 1.5     |
| Till, predominantly clay, brown, sandy, gravelly . . .                  | 1.5               | 1.5 - 3.0     |
| Silt, brown, sandy . . . . .  | 2.0               | 3.0 - 5.0     |
| Sand and gravel, gray, clayey, silty . . . . .                          | 7.0               | 5.0 - 12.0    |
| Till, predominantly clay, gray, silty, sandy, gravelly                  | 9.0               | 12.0 - 21.0   |
| Sand and gravel, gray . . . . .   | 3.0               | 21.0 - 24.0   |
| Till, predominantly clay, gray, pink cast, sandy,<br>gravelly . . . . . | 14.5              | 24.0 - 38.5   |
| Sand and gravel, gray, loosely packed . . . . .                         | 7.5               | 38.5 - 46.0   |
| Clay, gray . . . . .  | 1.0               | 46.0 - 47.0   |
| Sand and gravel, gray . . . . .   | 19.0              | 47.0 - 66.0   |
| Sand and gravel, brown, tight . . . . .                                 | 6.0               | 66.0 - 72.0   |
| Sand and gravel, brown . . . . .  | 35.5              | 72.0 - 107.5  |
| Sand and gravel, brown, loosely packed . . . . .                        | 4.5               | 107.5 - 112.0 |
| Sand and gravel, brown, small silt layers . . . . .                     | 14.0              | 112.0 - 126.0 |
| Dolomite, gray, shaly. . . . .  | 10.0              | 126.0 - 136.0 |
| Total depth 136.0 ft  |                   |               |

GAMMA-RAY LOG WITH DRILLER'S LITHOLOGY



KNE 38N6E-23.3h - Continued

SPLIT-SPOON SAMPLES

| Sample | Depth<br>(ft) | Recovery<br>(in.) | Blows/6-inch<br>hammer drop | N value* | Qp†<br>(tons/ft <sup>2</sup> ) | Moisture<br>content (%) |
|--------|---------------|-------------------|-----------------------------|----------|--------------------------------|-------------------------|
| 1      | 1.0 - 2.5     | 14                | 1- 3- 5                     | 8        | 1.0                            | 15.6                    |
| 2      | 3.0 - 4.5     | 10                | 4- 5- 9                     | 14       | --                             | 21.4                    |
| 3      | 10.0 - 11.5   | 6                 | 6- 3- 3                     | 6        | --                             | 14.0                    |
| 4      | 20.0 - 21.5   | 12                | 7- 8- 21                    | 29       | --                             | 11.8                    |
| 5      | 30.0 - 31.5   | 18                | 6- 7- 9                     | 16       | 2.3                            | 13.0                    |
| 6      | 40.0 - 41.5   | 14                | 15- 20- 20                  | 40       | --                             | --                      |
| 7      | 50.0 - 51.5   | 15                | 14- 17- 17                  | 34       | --                             | --                      |
| 8      | 60.0 - 61.5   | 13                | 16- 15- 11                  | 26       | --                             | --                      |
| 9      | 70.0 - 71.5   | 5                 | 19- 31- 26                  | 57       | --                             | --                      |
| 10     | 80.0 - 81.5   | 16                | 19- 28- 18                  | 46       | --                             | --                      |
| 11     | 90.0 - 91.5   | 10                | 13- 20- 22                  | 42       | --                             | --                      |
| 12     | 100.0 - 101.5 | 16                | 19- 24- 30                  | 54       | --                             | --                      |
| 13     | 110.0 - 111.5 | 10                | 19- 39- 42                  | 81       | --                             | --                      |
| 14     | 120.0 - 121.5 | 13                | 14- 42- 45                  | 97       | --                             | --                      |

\*Sum of hammer drops in last 12 inches.

†Unconfined compression strength measurement made with pocket penetrometer.

SIEVE AND HYDROMETER ANALYSES OF SPLIT-SPOON SAMPLES (in percent)

| Sample            | Distribution of all parts |                  | Distribution of part < 2.0 mm |                  |           |
|-------------------|---------------------------|------------------|-------------------------------|------------------|-----------|
|                   | > 2.0 mm                  | < 2.0 mm         | .062-<br>2.0 mm               | .004-<br>.062 mm | < .004 mm |
|                   | Gravel                    | Sand, silt, clay | Sand                          | Silt             | Clay      |
| 1 (lower 0.75 ft) | 22                        | 78               | 32                            | 52               | 16        |
| 2                 | 11                        | 89               | 36                            | 48               | 16        |
| 3                 | 12                        | 88               | 44                            | 41               | 15        |
| 4 (upper 0.5 ft)  | 12                        | 88               | 50                            | 36               | 14        |
| 5                 | 2                         | 98               | 35                            | 39               | 26        |

KNE 38N6E-23.3h - Concluded

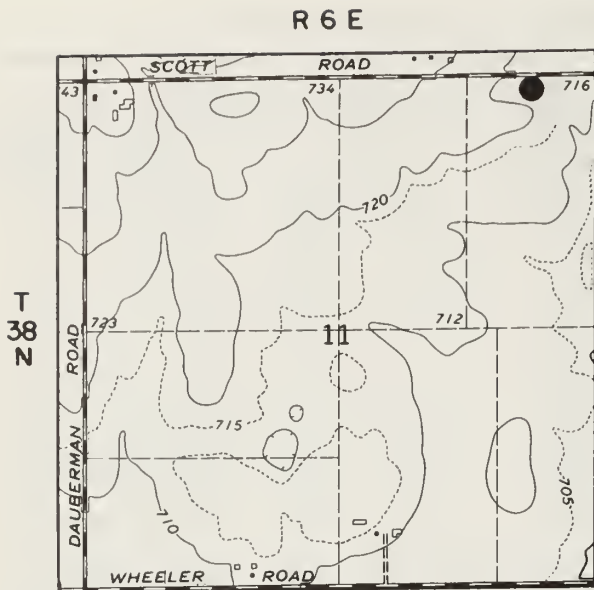
SIEVE ANALYSES OF SPLIT-SPOON SAMPLES (in cumulative percent)

| Sample no.<br>and depth<br>(ft)      | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|--------------------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                                      | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                                      | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| <sup>6</sup> <sub>40.0 - 41.5</sub>  | 17.9                | 36.5 | 52.3 | 60.6 | 63.1 | 75.1 | 84.1 | 87.8 | 90.4 | 92.4 | 93.2 | 100.0      |
| <sup>7</sup> <sub>50.0 - 51.5</sub>  | 30.5                | 50.1 | 60.0 | 65.3 | 70.6 | 78.5 | 85.0 | 88.0 | 90.6 | 92.6 | 93.7 | 100.0      |
| <sup>8</sup> <sub>60.0 - 61.5</sub>  | 9.4                 | 23.3 | 30.3 | 33.9 | 39.7 | 62.5 | 86.4 | 93.0 | 95.7 | 97.0 | 97.6 | 100.0      |
| <sup>10</sup> <sub>80.0 - 81.5</sub> | 15.7                | 26.5 | 36.9 | 43.4 | 51.6 | 67.8 | 80.6 | 85.7 | 89.0 | 91.6 | 93.2 | 100.0      |
| <sup>11</sup> <sub>90.0 - 91.5</sub> | 1.3                 | 6.7  | 17.8 | 30.5 | 47.6 | 65.9 | 74.6 | 78.9 | 83.2 | 86.0 | 90.4 | 100.0      |
| <sup>12</sup> <sub>100.0-101.5</sub> | 34.9                | 50.3 | 63.0 | 71.0 | 78.4 | 93.1 | 97.3 | 98.7 | 99.3 | 99.5 | 99.6 | 100.0      |
| <sup>13</sup> <sub>110.0-111.5</sub> | 6.0                 | 10.7 | 14.9 | 20.1 | 35.2 | 65.7 | 81.1 | 87.2 | 90.6 | 92.6 | 93.7 | 100.0      |
| <sup>14</sup> <sub>120.0-121.5</sub> | 32.4                | 51.4 | 64.3 | 70.3 | 75.2 | 80.1 | 83.7 | 86.2 | 88.6 | 90.5 | 91.7 | 100.0      |

SIEVE ANALYSES OF ROTARY SAMPLES (in cumulative percent)

| Sample<br>depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|-------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                         | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                         | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| 50.0- 55.0              | 26.4                | 63.8 | 80.0 | 85.5 | 90.2 | 94.5 | 97.3 | 98.5 | 99.1 | 99.4 | 99.6 | 100.0      |
| 60.0- 65.0              | 3.0                 | 35.7 | 63.8 | 73.8 | 81.1 | 90.1 | 95.6 | 97.4 | 98.4 | 98.9 | 99.1 | 100.0      |
| 70.0- 75.0              | 42.1                | 65.3 | 78.0 | 84.1 | 89.3 | 94.2 | 97.3 | 98.6 | 99.3 | 99.6 | 99.7 | 100.0      |
| 80.0- 85.0              | 22.8                | 51.1 | 72.4 | 80.8 | 86.5 | 92.6 | 96.3 | 98.0 | 98.8 | 99.2 | 99.4 | 100.0      |
| 90.0- 95.0              | 61.2                | 75.4 | 84.5 | 88.6 | 92.6 | 96.1 | 98.1 | 98.8 | 99.2 | 99.3 | 99.4 | 100.0      |
| 100.0-105.0             | 33.3                | 56.3 | 71.2 | 78.3 | 85.4 | 92.1 | 96.6 | 98.2 | 98.9 | 99.3 | 99.5 | 100.0      |
| 110.0-115.0             | 31.8                | 53.3 | 63.3 | 69.8 | 78.6 | 89.5 | 95.9 | 98.2 | 99.1 | 99.4 | 99.5 | 100.0      |
| 120.0-125.0             | 26.5                | 59.7 | 74.2 | 78.8 | 84.3 | 91.0 | 95.8 | 97.8 | 98.8 | 99.2 | 99.4 | 100.0      |

DRILLING RECORD FOR KNE 38N6E-11.1h



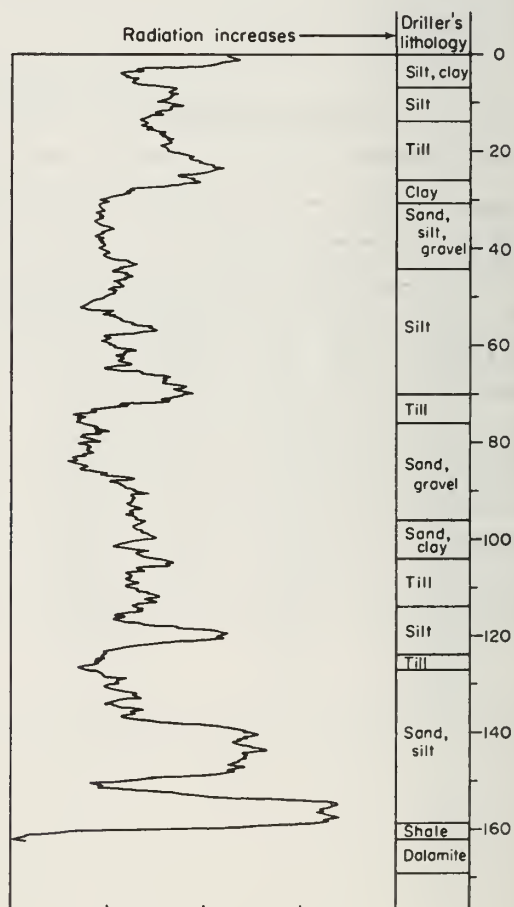
Location of test:

N 5,250 ft, W 650 ft from SE cor. of sec. 11, S 30 ft of the center line and W 650 ft of a 24-in. metal culvert pipe under Scott Road (Big Rock Quadrangle, 1968)

Surface elevation: 718 ft  
 Date started: 6-21-72  
 Date completed: 6-23-72  
 Electric log interval: 0-163.0 ft  
 Natural gamma log interval: 0-162.0 ft

Remarks: Flow of 0.5 gpm (gallons per minute) developed overnight from the mud-filled borehole 150.0 ft deep.

GAMMA-RAY LOG WITH DRILLER'S LITHOLOGY





DESCRIPTION OF MATERIALS

| Description   | Thickness<br>(ft) | Depth<br>(ft) |
|---|-------------------|---------------|
| Topsoil, black . . . . .  | 1.5               | 0.0 - 1.5     |
| Silt, gray, sandy, boulders . . . . .                                     | 1.5               | 1.5 - 3.0     |
| Clay, brown and gray, sandy, sand and gravel seams . .                    | 2.0               | 3.0 - 5.0     |
| Sand and gravel, brown . . . . .  | 2.0               | 5.0 - 7.0     |
| Silt, gray, clayey . . . . .  | 7.0               | 7.0 - 14.0    |
| Sand and gravel, gray . . . . .   | 1.0               | 14.0 - 15.0   |
| Till, predominantly clay, gray, pink cast, sandy,<br>gravelly . . . . .   | 11.0              | 15.0 - 26.0   |
| Clay, gray, silty . . . . .   | 4.5               | 26.0 - 30.5   |
| Sand, brown, silty, loosely packed . . . . .                              | 3.5               | 30.5 - 34.0   |
| Silt, brown, clayey . . . . .   | 3.0               | 34.0 - 37.0   |
| Sand and gravel, brown, clay layers . . . . .                             | 7.0               | 37.0 - 44.0   |
| Silt, gray, sand and gravel layers . . . . .                              | 13.0              | 44.0 - 57.0   |
| Silt, gray, clayey, sandy . . . . .                                       | 13.0              | 57.0 - 70.0   |
| Till, predominantly clay, gray, sandy, silty, gravelly                    | 6.0               | 70.0 - 76.0   |
| Sand and gravel, brown . . . . .  | 20.0              | 76.0 - 96.0   |
| Clay, gray, sandy . . . . .   | 2.0               | 96.0 - 98.0   |
| Sand, brown, silty . . . . .  | 6.0               | 98.0 - 104.0  |
| Till, predominantly clay, gray, sandy, gravelly,<br>sand layers . . . . . | 10.0              | 104.0 - 114.0 |
| Silt, gray, hard . . . . .  | 10.0              | 114.0 - 124.0 |
| Till, predominantly clay, gray, sandy, gravelly . . .                     | 3.0               | 124.0 - 127.0 |
| Sand, gray, silty, hard . . . . .   | 11.0              | 127.0 - 138.0 |
| Silt, gray, clayey, hard . . . . .  | 14.0              | 138.0 - 152.0 |
| Sand, gray . . . . .  | 7.0               | 152.0 - 159.0 |
| Shale, gray . . . . .   | 3.0               | 159.0 - 162.0 |
| Dolomite, gray . . . . .  | 7.0               | 162.0 - 169.0 |
| Total depth 169.0 ft  |                   |               |

KNE 38N6E-11.1h - Continued

SPLIT-SPOON SAMPLES

| Sample | Depth<br>(ft) | Recovery<br>(in.) | Blows/6-inch<br>hammer drop | N value* | Qp†<br>(tons/ft <sup>2</sup> ) | Moisture<br>content (%) |
|--------|---------------|-------------------|-----------------------------|----------|--------------------------------|-------------------------|
| 1      | 1.0 - 2.5     | 9                 | 2- 2- 4                     | 6        | 1.5                            | 26.2                    |
| 2      | 3.0 - 4.5     | 18                | 3- 4- 4                     | 8        | 1.0                            | 15.7                    |
| 3      | 5.0 - 6.5     | 15                | 5- 9- 11                    | 20       | 4.0                            | 15.2                    |
| 4      | 10.0 - 11.5   | 12                | 8- 13- 16                   | 29       | 4.5+                           | 14.7                    |
| 5      | 20.0 - 21.5   | 18                | 5- 6- 7                     | 13       | 0.8                            | 11.1                    |
| 6      | 30.0 - 31.5   | 15                | 5- 9- 9                     | 18       | --                             | 24.7                    |
| 7      | 40.0 - 41.5   | 18                | 5- 10- 13                   | 23       | --                             | 19.4                    |
| 8      | 50.0 - 51.5   | 15                | 17- 24- 27                  | 51       | --                             | 24.4                    |
| 9      | 60.0 - 61.5   | 18                | 21- 41- 32                  | 73       | 4.5+                           | 9.4                     |
| 10     | 70.0 - 71.5   | 13                | 10- 21- 34                  | 55       | 3.8                            | 12.1                    |
| 11     | 80.0 - 81.5   | 18                | 31- 55- 74                  | 129      | --                             | --                      |
| 12     | 90.0 - 91.5   | 18                | 45- 55- 50                  | 105      | --                             | 15.8                    |
| 13     | 105.0 - 106.5 | 18                | 16- 23- 41                  | 64       | 2.8                            | 10.4                    |
| 14     | 110.0 - 111.5 | 11                | 11- 20- 21                  | 41       | 3.5                            | 8.2                     |
| 15     | 120.0 - 121.5 | 16                | 14- 29- 39                  | 68       | 4.5+                           | 15.0                    |
| 16     | 130.0 - 131.5 | 17                | 44- 70- 81                  | 151      | --                             | --                      |
| 17     | 140.0 - 141.5 | 14                | 21- 39- 48                  | 87       | 4.5+                           | 13.5                    |
| 18     | 150.0 - 151.5 | 18                | 38- 42- 61                  | 103      | 4.5+                           | 13.4                    |
| 19     | 160.0 - 160.5 | 3                 | 131 (6-in. total drop)      | --       | --                             | 10.0                    |

\* Sum of hammer drops in last 12 inches.

† Unconfined compressive strength measurement made with pocket penetrometer.

SIEVE AND HYDROMETER ANALYSES OF SPLIT-SPOON SAMPLES (in percent)

| Sample | Distribution of all parts |                  | Distribution of part < 2.0 mm |                  |           |
|--------|---------------------------|------------------|-------------------------------|------------------|-----------|
|        | > 2.0 mm                  | < 2.0 mm         | .062-<br>2.0 mm               | .004-<br>.062 mm | < .004 mm |
|        | Gravel                    | Sand, silt, clay | Sand                          | Silt             | Clay      |
| 2      | 5                         | 95               | 40                            | 49               | 11        |
| 3      | 6                         | 94               | 16                            | 69               | 15        |
| 4      | 3                         | 97               | 18                            | 63               | 19        |
| 5      | 4                         | 96               | 29                            | 42               | 29        |
| 9      | 8                         | 92               | 53                            | 33               | 14        |
| 10     | 1                         | 99               | 12                            | 82               | 6         |
| 12     | 7                         | 93               | 38                            | 30               | 32        |
| 13     | 9                         | 91               | 40                            | 39               | 21        |
| 14     | 12                        | 88               | 48                            | 36               | 16        |
| 15     | 0                         | 100              | 6                             | 62               | 32        |
| 17     | 0                         | 100              | 3                             | 65               | 32        |
| 18     | 0                         | 100              | 5                             | 66               | 29        |

KNE 38N6E-11.1h - Concluded

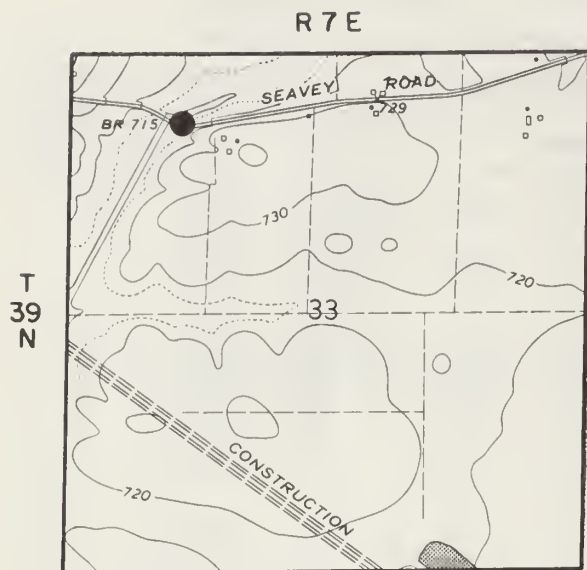
SIEVE ANALYSES OF SPLIT-SPOON SAMPLES (in cumulative percent)

| Sample no.<br>and depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|---------------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                                 | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                                 | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| <sup>7</sup> 40.0 - 41.5        | 0.9                 | 1.5  | 3.1  | 3.5  | 3.9  | 11.4 | 54.6 | 80.4 | 89.7 | 92.6 | 94.2 | 100.0      |
| <sup>11</sup> 60.0 - 61.5       | 6.0                 | 15.9 | 23.4 | 27.5 | 31.8 | 40.2 | 51.7 | 62.0 | 74.5 | 84.3 | 90.0 | 100.0      |
| <sup>12</sup> 80.0 - 81.5       | 1.4                 | 3.9  | 7.6  | 11.0 | 20.4 | 43.6 | 70.3 | 83.7 | 86.4 | 88.1 | 94.4 | 100.0      |
| <sup>16</sup> 130.0-131.5       | 0.0                 | 0.8  | 1.6  | 3.1  | 6.0  | 12.9 | 31.5 | 66.1 | 83.9 | 90.5 | 93.4 | 100.0      |

SIEVE ANALYSES OF ROTARY SAMPLES (in cumulative percent)

| Sample<br>depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |       |
|-------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|-------|
|                         | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan   |
|                         | Gravel              |      | Sand |      |      |      |      |      |      |      |      |       |
| 40.0- 45.0              | 0.8                 | 4.0  | 4.8  | 8.8  | 19.0 | 33.8 | 62.3 | 79.3 | 88.9 | 93.3 | 95.1 | 100.0 |
| 80.0- 85.0              | 1.7                 | 6.1  | 15.7 | 19.6 | 27.9 | 43.4 | 70.4 | 84.5 | 92.9 | 96.5 | 97.7 | 100.0 |
| 90.0- 95.0              | 0.1                 | 4.6  | 11.0 | 15.6 | 28.0 | 46.5 | 74.3 | 87.4 | 93.8 | 96.5 | 97.5 | 100.0 |
| 130.0-135.0             | 0.3                 | 11.4 | 18.6 | 22.5 | 31.4 | 45.3 | 71.2 | 85.9 | 93.4 | 96.2 | 97.4 | 100.0 |
| 150.0-155.0             | 0.0                 | 7.1  | 16.8 | 19.5 | 24.8 | 35.2 | 58.1 | 75.1 | 86.0 | 91.4 | 94.3 | 100.0 |

DRILLING RECORD FOR KNE 39N7E-33.7g



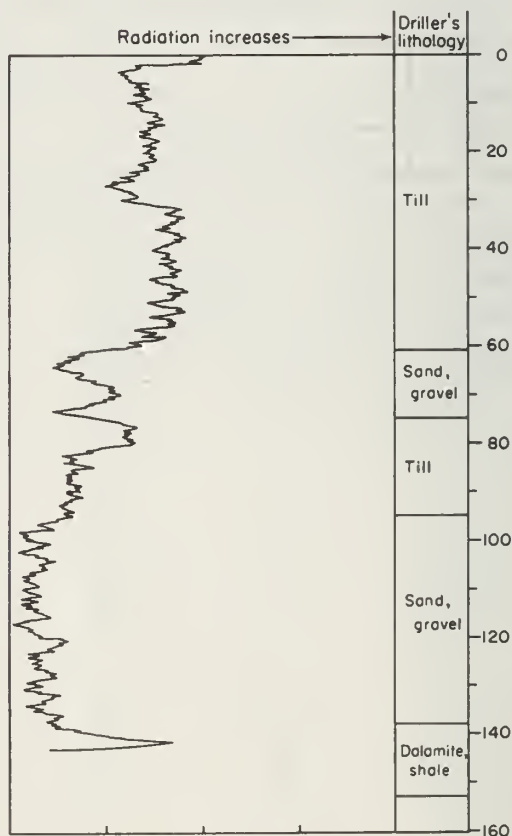
Location of test:

N 4,600 ft, W 4,100 ft from  
SE cor. of sec. 33, N 20 ft  
of the center line of Seavey  
Road and E 290 ft of the center  
of a concrete bridge along  
Seavey Road (Sugar Grove  
Quadrangle, 1964)

Surface elevation: 715 ft  
Date started: 6-26-72  
Date completed: 6-28-72  
Electric log interval: 0-142.0 ft  
Natural gamma log interval: 0-143.0 ft

Zones of fluid loss:  
61.0-67.0 ft  
Density: 10.2 lb/gal  
Viscosity: 44 sec/qt  
Loss: 120 gal  
115.0-121.0 ft  
Density: 9.8 lb/gal  
Viscosity: 75 sec/qt  
Loss: 65 gal

GAMMA-RAY LOG WITH DRILLER'S LITHOLOGY



KNE 39N7E-33.7g - Continued

DESCRIPTION OF MATERIALS

| Description  | Thickness<br>(ft) | Depth<br>(ft) |
|--|-------------------|---------------|
| Topsoil, black . . . . .   | 1.0               | 0.0 - 1.0     |
| Till, predominantly clay, brown, sandy, silty,<br>gravelly . . . . .                 | 2.5               | 1.0 - 3.5     |
| Till, predominantly clay, gray, pink cast, sandy,<br>gravelly . . . . .              | 2.5               | 3.5 - 6.0     |
| Till, predominantly clay, gray, sandy, gravelly, sand<br>and gravel layers . . . . . | 24.0              | 6.0 - 30.0    |
| Till, predominantly clay, gray, sandy, gravelly, hard                                | 31.0              | 30.0 - 61.0   |
| Sand and gravel, gray . . . . .  | 6.0               | 61.0 - 67.0   |
| Sand and gravel, gray, clay layers . . . . .   | 7.5               | 67.0 - 74.5   |
| Till, predominantly clay, gray, sandy, gravelly,<br>very hard . . . . .              | 9.5               | 74.5 - 84.0   |
| Till, predominantly clay, gray, sandy, gravelly . . .                                | 11.0              | 84.0 - 95.0   |
| Sand and gravel, brown, boulders . . . . .   | 43.0              | 95.0 - 138.0  |
| Dolomite, gray . . . . .   | 3.0               | 138.0 - 141.0 |
| Dolomite and shale, green . . . . .  | 12.0              | 141.0 - 153.0 |
| Total depth 153.0 ft   |                   |               |

SPLIT-SPOON SAMPLES

| Sample | Depth<br>(ft) | Recovery<br>(in.) | Blows/6-inch<br>hammer drop* | N value† | Qp‡<br>(tons/ft²) | Moisture<br>content (%) |      |
|--------|---------------|-------------------|------------------------------|----------|-------------------|-------------------------|------|
| 1      | 1.0 - 2.5     | 9                 | 3- 4- 6                      | 10       | 1.8               | 29.0                    |      |
| 2      | 5.0 - 6.5     | 16                | 7- 4- 4                      | 8        | 1.5               | 13.2                    |      |
| 3      | 10.0 - 11.5   | 11                | 3- 5- 7                      | 12       | 2.0               | 12.7                    |      |
| 4      | 20.0 - 21.5   | 16                | 8- 26- 38                    | 64       | 4.5+              | 8.3                     |      |
| 5      | 30.0 - 31.5   | 16                | 22- 27- 22                   | 49       | 4.5+              | 8.2                     |      |
| 6      | 40.0 - 41.5   | 18                | 20- 36- 51                   | 87       | 4.5+              | 9.0                     |      |
| 7      | 50.0 - 51.5   | 18                | 15- 28- 40                   | 68       | 4.5+              | 10.5                    |      |
| 8      | 60.0 - 61.5   | 10                | 4- 5- 7                      | 12       | 3.3               | 12.8                    |      |
| 9      | 70.0 - 71.5   | 14                | 14- 15- 18                   | 33       | --                | 12.1                    |      |
| 10     | 80.0 - 80.8   | 8                 | 66-100 (10-in. total drop)   |          |                   | 4.5+                    | 11.7 |
| 11     | 90.0 - 91.5   | 8                 | 32- 53-103                   | 156      | 4.5+              | 11.7                    |      |
| 12     | 97.0 - 97.5   | 6                 | 150- 31                      | --       | --                | 11.6                    |      |
| 13     | 110.0 - 111.5 | 4                 | 51-109-162                   | 271      | --                | 12.1                    |      |
| 14     | 115.0 - 115.6 | 7                 | 170- 50 (7-in. total drop)   |          |                   | --                      | 13.4 |
| 15     | 121.0 - 122.5 | 11                | 22- 48- 55                   | 103      | --                | --                      |      |
| 16     | 130.0 - 131.5 | 16                | 66-159-124                   | 283      | --                | 12.2                    |      |

\* Sample 12 (last 6 inches) and sample 14 (last 7 inches) - 300 lb hammer.

† Sum of hammer drops in last 12 inches.

‡ Unconfined compressive strength measurement made with pocket penetrometer.



KNE 39N7E-33.7g - Concluded

SIEVE AND HYDROMETER ANALYSES OF SPLIT-SPOON SAMPLES (in percent)

| Sample | Distribution of all parts |                  | Distribution of part < 2.0 mm |                  |           |
|--------|---------------------------|------------------|-------------------------------|------------------|-----------|
|        | > 2.0 mm                  | < 2.0 mm         | .062-<br>2.0 mm               | .004-<br>.062 mm | < .004 mm |
|        | Gravel                    | Sand, silt, clay | Sand                          | Silt             | Clay      |
| 2      | 6                         | 94               | 25                            | 44               | 31        |
| 3      | 4                         | 96               | 33                            | 37               | 30        |
| 4      | 7                         | 93               | 42                            | 33               | 25        |
| 5      | 4                         | 96               | 31                            | 38               | 31        |
| 6      | 0                         | 100              | 8                             | 72               | 20        |
| 7      | 3                         | 97               | 27                            | 45               | 28        |
| 8      | 3                         | 97               | 26                            | 42               | 32        |
| 10     | 15                        | 85               | 33                            | 43               | 24        |
| 11     | 12                        | 88               | 36                            | 43               | 21        |

SIEVE ANALYSES OF SPLIT-SPOON SAMPLES (in cumulative percent)

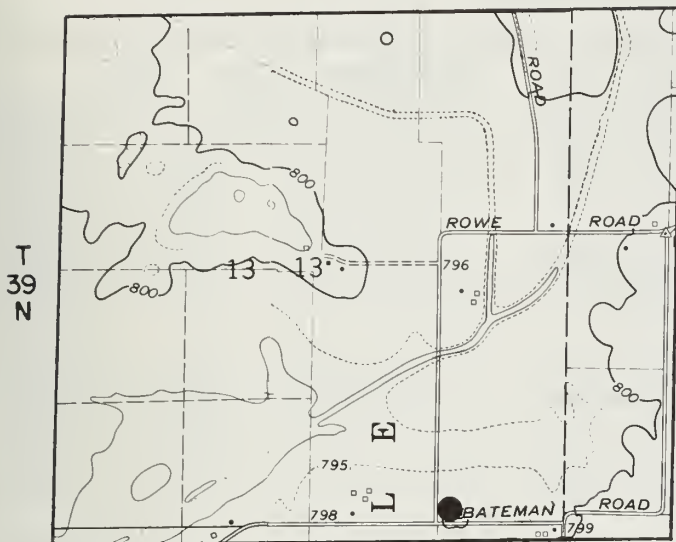
| Sample no.<br>and depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|---------------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                                 | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                                 | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| <sup>8</sup> 60.0 - 61.5        | 5.4                 | 13.0 | 23.0 | 30.6 | 39.1 | 53.2 | 70.3 | 81.1 | 89.8 | 94.2 | 95.9 | 100.0      |
| <sup>9</sup> 70.0 - 71.5        | 28.1                | 51.8 | 68.8 | 75.8 | 80.2 | 83.8 | 86.3 | 88.1 | 90.2 | 92.0 | 93.0 | 100.0      |
| <sup>15</sup> 121.0-122.5       | 11.0                | 28.4 | 43.8 | 53.1 | 62.9 | 74.0 | 81.3 | 84.9 | 88.4 | 90.0 | 92.2 | 100.0      |
| <sup>16</sup> 130.0-131.5       | 31.3                | 50.9 | 66.1 | 73.0 | 77.6 | 81.5 | 84.1 | 86.0 | 88.2 | 90.1 | 91.3 | 100.0      |

SIEVE ANALYSES OF ROTARY SAMPLES (in cumulative percent)

| Sample<br>depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |       |
|-------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|-------|
|                         | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan   |
|                         | Gravel              |      | Sand |      |      |      |      |      |      |      |      |       |
| 60.0- 65.0              | 28.6                | 60.9 | 82.6 | 88.1 | 93.1 | 96.2 | 98.0 | 98.7 | 99.1 | 99.3 | 99.4 | 100.0 |
| 70.0- 75.0              | 31.8                | 77.3 | 89.5 | 91.8 | 93.9 | 95.4 | 96.6 | 97.3 | 97.8 | 98.2 | 98.5 | 100.0 |
| 90.0- 95.0              | 78.0                | 89.1 | 93.5 | 95.5 | 97.2 | 98.7 | 99.2 | 99.5 | 99.6 | 99.7 | 99.8 | 100.0 |
| 110.0-115.0             | 43.0                | 77.5 | 92.2 | 94.6 | 96.4 | 97.5 | 98.5 | 99.0 | 99.3 | 99.4 | 99.5 | 100.0 |
| 120.0-125.0             | 51.8                | 82.9 | 92.8 | 95.0 | 96.8 | 97.9 | 98.9 | 99.3 | 99.5 | 99.6 | 99.7 | 100.0 |
| 130.0-135.0             | 24.7                | 51.1 | 75.6 | 84.7 | 92.7 | 96.5 | 98.5 | 99.1 | 99.4 | 99.5 | 99.6 | 100.0 |

DRILLING RECORD FOR KNE 39N6E-13.3a

R 6 E



Location of text:

N 75 ft, W 1,340 ft from SE cor. of sec. 13, N 75 ft and E 20 ft of intersection of center lines of Bateman and Rowe Roads (Sugar Grove Quadrangle, 1964)

Surface elevation: 798 ft  
 Date started: 6-15-72  
 Date completed: 6-19-72  
 Electric log interval: 0-142.0 ft  
 Natural gamma log interval: 0-142.0 ft

GAMMA-RAY LOG WITH DRILLER'S LITHOLOGY

Zones of fluid loss:

59.0-66.0 ft

Density: 9.8 lb/gal  
 Viscosity: 40 sec/qt  
 Loss: 570 gal

66.0-70.0 ft

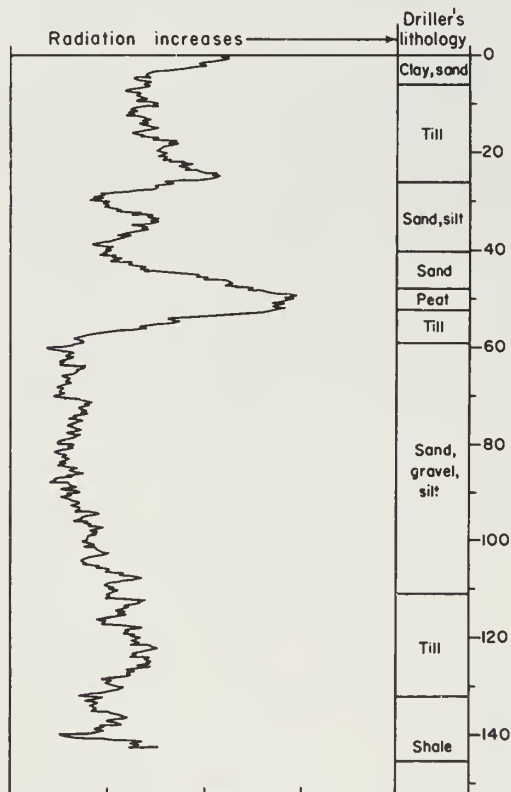
Density: 9.8 lb/gal  
 Viscosity: 42 sec/qt  
 Loss: 90 gal

70.0-74.0 ft

Density: 9.8 lb/gal  
 Viscosity: 42 sec/qt  
 Loss: 30 gal

74.0-93.0 ft

Density: 9.8 lb/gal  
 Viscosity: 42 sec/qt  
 Loss: 285 gal



KNE 39N6E-13.3a - Continued

DESCRIPTION OF MATERIALS

| Description   | Thickness<br>(ft) | Depth<br>(ft) |
|---|-------------------|---------------|
| Topsoil, black . . . . .  | 1.0               | 0.0 - 1.0     |
| Clay, brown, sandy . . . . .  | 3.0               | 1.0 - 4.0     |
| Sand, brown, silty . . . . .  | 2.0               | 4.0 - 6.0     |
| Till, predominantly clay, brown, silty, gravelly . . .                                      | 20.0              | 6.0 - 26.0    |
| Silt, gray, clayey . . . . .  | 3.0               | 26.0 - 29.0   |
| Sand, brown . . . . .   | 4.0               | 29.0 - 33.0   |
| Silt, gray, sandy, soft . . . . .   | 3.0               | 33.0 - 36.0   |
| Sand, gray, silty, gravelly . . . . .   | 4.0               | 36.0 - 40.0   |
| Till, predominantly clay, gray, gravelly . . . . .  | 2.0               | 40.0 - 42.0   |
| Sand, gray, clay layers . . . . .   | 5.5               | 42.0 - 47.5   |
| Peat . . . . .  | 4.0               | 47.5 - 51.5   |
| Clay, gray, organic material, hard . . . . .  | 3.5               | 51.5 - 54.0   |
| Till, predominantly clay, gray, sandy, gravelly . . .                                       | 5.0               | 54.0 - 59.0   |
| Sand and gravel, gray, boulders . . . . .   | 7.0               | 59.0 - 66.0   |
| Silt, gray, sandy, gravelly . . . . .   | 8.0               | 66.0 - 74.0   |
| Sand and gravel, gray . . . . .   | 32.0              | 74.0 - 106.0  |
| Silt, gray, clayey . . . . .  | 3.0               | 106.0 - 109.0 |
| Sand and gravel, brown . . . . .  | 2.0               | 109.0 - 111.0 |
| Till, predominantly clay, gray, sandy, silty, gravelly                                      | 15.0              | 111.0 - 126.0 |
| Till, predominantly clay, gray, sandy, silty,<br>gravelly, sand and gravel layers . . . . . | 6.0               | 126.0 - 132.0 |
| Shale, green, silty; dolomite, gray, broken . . . . .                                       | 3.0               | 132.0 - 135.0 |
| Shale, green, silty; dolomite, gray . . . . .   | 10.0              | 135.0 - 145.0 |
| Total depth 145.0 ft  |                   |               |

KNE 39N6E-13.3a - Continued

SPLIT-SPOON SAMPLES

| Sample | Depth<br>(ft) | Recovery<br>(in.) | Blows/6-inch<br>hammer drop | N value* | Qp†<br>(tons/ft <sup>2</sup> ) | Moisture<br>content (%) |
|--------|---------------|-------------------|-----------------------------|----------|--------------------------------|-------------------------|
| 1      | 1.0 - 2.5     | 14                | 2- 2- 4                     | 6        | 1.0 <sup>1</sup>               | 28.4 <sup>2</sup>       |
| 2      | 3.0 - 4.5     | 14                | 2- 3- 5                     | 8        | --                             | 23.2                    |
| 3      | 10.0 - 11.5   | 18                | 5- 7- 9                     | 16       | 1.5                            | 11.4                    |
| 4      | 20.0 - 21.5   | 18                | 3- 7- 9                     | 16       | 1.3                            | 10.9                    |
| 5      | 30.0 - 31.5   | 15                | 8- 16- 17                   | 32       | --                             | 20.2                    |
| 6      | 35.0 - 36.5   | 18                | 9- 12- 14                   | 26       | --                             | 20.1                    |
| 7      | 36.5 - 38.0   | 15                | 8- 12- 16                   | 28       | --                             | 18.3                    |
| 8      | 38.0 - 39.5   | 13                | 8- 14- 35                   | 49       | --                             | 19.6                    |
| 9      | 39.5 - 41.0   | 9                 | 28- 33- 19                  | 52       | 4.5+                           | 9.3                     |
| 10     | 41.0 - 42.5   | 9                 | 5- 3- 29                    | 32       | 2.5                            | 12.8                    |
| 11     | 42.5 - 44.0   | 10                | 17- 37- 41                  | 78       | --                             | 24.4                    |
| 12     | 44.0 - 45.5   | 9                 | 6- 35- 44                   | 79       | --                             | 15.6                    |
| 13     | 48.0 - 49.5   | 18                | 4- 6- 9                     | 15       | 2.3 <sup>3</sup>               | 47.6 <sup>4</sup>       |
| 14     | 49.5 - 51.0   | 15                | 10- 16- 23                  | 39       | 2.0                            | 21.6                    |
| 15     | 51.0 - 52.5   | 18                | 13- 20- 29                  | 49       | 4.5+                           | 15.2                    |
| 16     | 61.0 - 62.5   | 15                | 76- 55- 59                  | 114      | --                             | 16.0                    |
| 17     | 70.0 - 71.5   | 12                | 29- 27- 14                  | 41       | --                             | 16.3                    |
| 18     | 80.0 - 81.5   | 6                 | 16- 47- 36                  | 83       | --                             | 14.0                    |
| 19     | 90.0 - 91.5   | 18                | 26- 18- 15                  | 33       | --                             | 9.6                     |
| 20     | 100.0 - 101.5 | 15                | 22- 29- 31                  | 60       | --                             | 16.9                    |
| 21     | 110.0 - 111.0 | 8                 | 66-109                      | --       | --                             | 14.8                    |
| 22     | 120.0 - 121.5 | 18                | 12- 13- 19                  | 32       | 2.0                            | 10.5                    |
| 23     | 130.0 - 131.5 | 15                | 26- 37- 87                  | 124      | 4.0                            | 15.0                    |

\* Sum of hammer drops in last 12 inches.

† Unconfined compressive strength measurement made with pocket penetrometer.

<sup>1</sup>Lower 9 inches.    <sup>2</sup>Lower 9 inches.    <sup>3</sup>Upper inch.    <sup>4</sup>Lower 14 inches.

KNE 39N6E-13.3a - Continued

SIEVE AND HYDROMETER ANALYSES OF SPLIT-SPOON SAMPLES (in percent)

| Sample          | Distribution of all parts |                  | Distribution of part < 2.0 mm |                  |           |
|-----------------|---------------------------|------------------|-------------------------------|------------------|-----------|
|                 | > 2.0 mm                  | < 2.0 mm         | .062-<br>2.0 mm               | .004-<br>.062 mm | < .004 mm |
|                 | Gravel                    | Sand, silt, clay | Sand                          | Silt             | Clay      |
| 1 <sup>1</sup>  | 0                         | 100              | 7                             | 52               | 41        |
| 2               | 0                         | 100              | 72                            | 22               | 6         |
| 3               | 8                         | 92               | 45                            | 42               | 13        |
| 4               | 7                         | 93               | 33                            | 49               | 18        |
| 5               | 0                         | 100              | 66                            | 23               | 11        |
| 6               | 0                         | 100              | 48                            | 42               | 10        |
| 7               | 0                         | 100              | 71                            | 21               | 8         |
| 8               | 0                         | 100              | 58                            | 34               | 8         |
| 9               | 21                        | 79               | 45                            | 33               | 22        |
| 10              | 23                        | 67               | 55                            | 20               | 25        |
| 11              | 1                         | 99               | 67                            | 27               | 6         |
| 12              | 1                         | 99               | 44                            | 43               | 13        |
| 13 <sup>2</sup> | 0                         | 100              | 8                             | 56               | 36        |
| 13 <sup>3</sup> | 0                         | 100              | 8                             | 63               | 29        |
| 14              | 0                         | 94               | 6                             | 67               | 27        |
| 15              | 0                         | 100              | 8                             | 54               | 38        |
| 16              | 22                        | 78               | 79                            | 12               | 9         |
| 17              | 18                        | 72               | 60                            | 25               | 15        |
| 18              | 19                        | 71               | 67                            | 20               | 13        |

<sup>1</sup>Lower 9 in.    <sup>2</sup>Upper 4 in.    <sup>3</sup>Lower 14 in.

SIEVE ANALYSES OF SPLIT-SPOON SAMPLES (in cumulative percent)

| Sample no.<br>and depth<br>(ft) | Tyler screen number |     |      |      |      |      |      |      |      |      |      | Pan        |
|---------------------------------|---------------------|-----|------|------|------|------|------|------|------|------|------|------------|
|                                 | 4                   | 9   | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  |            |
|                                 | Gravel              |     | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| <sup>2</sup> 3.0 - 4.5          | 0.0                 | 0.1 | 0.2  | 0.3  | 0.7  | 1.5  | 5.7  | 27.1 | 64.2 | 85.3 | 90.8 | 100.0      |
| <sup>5</sup> 30.0 - 31.5        | 0.0                 | 0.5 | 0.9  | 1.4  | 1.8  | 2.4  | 4.6  | 12.9 | 42.5 | 70.5 | 82.4 | 100.0      |
| <sup>10</sup> 41.0 - 42.5       | 1.6                 | 3.8 | 6.5  | 9.0  | 14.4 | 31.1 | 58.9 | 78.8 | 91.0 | 94.9 | 96.0 | 100.0      |
| <sup>11</sup> 42.5 - 44.0       | 0.0                 | 0.0 | 0.0  | 0.2  | 0.5  | 1.2  | 3.4  | 12.7 | 46.5 | 69.5 | 78.8 | 100.0      |
| <sup>20*</sup> 100.0-101.5      | 2.3                 | 5.8 | 10.2 | 13.2 | 18.0 | 33.6 | 60.1 | 73.2 | 82.9 | 87.8 | 89.4 | 100.0      |
| <sup>23</sup> 130.0-131.5       | 0.1                 | 0.8 | 2.6  | 7.3  | 18.0 | 41.4 | 67.7 | 81.4 | 89.0 | 92.5 | 93.8 | 100.0      |

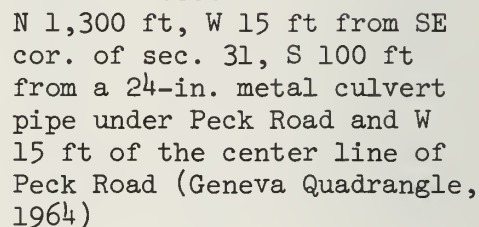
\* Lower 0.6 foot of interval only.



KNE 39N6E-13.3a - Concluded

SIEVE ANALYSES OF ROTARY SAMPLES (in cumulative percent)

| Sample<br>depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|-------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                         | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                         | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| 35.0- 40.0              | 1.7                 | 4.7  | 6.9  | 7.9  | 9.1  | 12.0 | 23.8 | 52.3 | 81.9 | 92.7 | 96.6 | 100.0      |
| 60.0- 65.0              | 7.6                 | 45.4 | 71.5 | 79.2 | 84.8 | 89.5 | 92.3 | 94.4 | 96.8 | 95.0 | 98.5 | 100.0      |
| 70.0- 75.0              | 21.5                | 37.8 | 60.0 | 71.7 | 80.2 | 88.1 | 92.3 | 94.3 | 96.1 | 97.2 | 97.8 | 100.0      |
| 80.0- 85.0              | 61.5                | 77.9 | 87.4 | 91.6 | 95.2 | 97.5 | 98.3 | 98.7 | 99.0 | 99.2 | 99.4 | 100.0      |
| 90.0- 95.0              | 78.0                | 89.1 | 93.5 | 95.5 | 97.2 | 98.7 | 99.2 | 99.5 | 99.6 | 99.7 | 99.8 | 100.0      |
| 100.0-105.0             | 9.6                 | 17.2 | 26.3 | 35.7 | 48.7 | 70.0 | 88.1 | 94.7 | 97.6 | 98.7 | 99.1 | 100.0      |



GAMMA-RAY LOG WITH DRILLER'S LITHOLOGY

Radiation increases →

Driller's lithology

0

Soil, clay

Till

Sand, gravel

20

Till

Sand, gravel

40

Till

60

Dolomite, shale

80

KNE 40N8E-31.1b - Continued

DESCRIPTION OF MATERIALS

| Description   | Thickness<br>(ft) | Depth<br>(ft) |
|---|-------------------|---------------|
| Topsoil, black . . . . .  | 1.5               | 0.0 - 1.5     |
| Clay, brown, sandy . . . . .  | 3.5               | 1.5 - 5.0     |
| Till, predominantly clay, gray, sandy, gravelly . . .                   | 8.0               | 5.0 - 13.0    |
| Clay, gray, sandy . . . . .   | 1.0               | 13.0 - 14.0   |
| Sand and gravel, brown . . . . .  | 7.0               | 14.0 - 21.0   |
| Till, clay, gray, sandy, gravelly . . . . .                             | 3.0               | 21.0 - 24.0   |
| Sand and gravel, gray, clayey . . . . .                                 | 10.0              | 24.0 - 34.0   |
| Till, predominantly clay, gray, pink cast, sandy,<br>gravelly . . . . . | 15.0              | 34.0 - 49.0   |
| Till, predominantly clay, gray, sandy, gravelly, hard.                  | 19.0              | 49.0 - 68.0   |
| Dolomite, brown; shale, green; clay, white . . . . .                    | 14.0              | 68.0 - 82.0   |
| Total depth 82.0 ft   |                   |               |

SPLIT-SPOON SAMPLES

| Sample | Depth<br>(ft) | Recovery<br>(in.) | Blows/6-inch<br>hammer drop | N value* | Q <sub>pt</sub><br>(tons/ft <sup>2</sup> ) | Moisture<br>content (%) |
|--------|---------------|-------------------|-----------------------------|----------|--|-------------------------|
| 1      | 1.0 - 2.5     | 9                 | 2- 4- 7                     | 11       | 4.3  | 20.5                    |
| 2      | 3.0 - 4.5     | 15                | 3- 4- 6                     | 10       | 1.5  | 28.2                    |
| 3      | 10.0 - 11.5   | 18                | 4- 7- 8                     | 15       | 2.5  | 14.9                    |
| 4      | 20.0 - 21.5   | 14                | 6- 8- 11                    | 19       | 1.0  | 16.0†                   |
| 5      | 30.0 - 31.5   | 6                 | 6- 11- 24                   | 35       | --   | --                      |
| 6      | 40.0 - 41.5   | 6                 | 4- 6- 70                    | 76       | 4.5+                                       | 10.9                    |
| 7      | 50.0 - 51.5   | 8                 | 14- 21- 52                  | 73       | 4.5+                                       | 11.1                    |
| 8      | 60.0 - 61.5   | 12                | 22- 31- 46                  | 77       | 4.5+                                       | 10.9                    |
| 9      | 70.0 - 71.5   | 15                | 47- 76- 81                  | 157      | 4.5+                                       | 19.3                    |

\*Sum of hammer drops in last 12 inches.

†Unconfined compressive strength measurement made with pocket penetrometer.

‡For interval 20.0 - 20.4 ft only.

KNE 40N8E-31.1b - Concluded

SIEVE AND HYDROMETER ANALYSES OF SPLIT-SPOON SAMPLES (in percent)

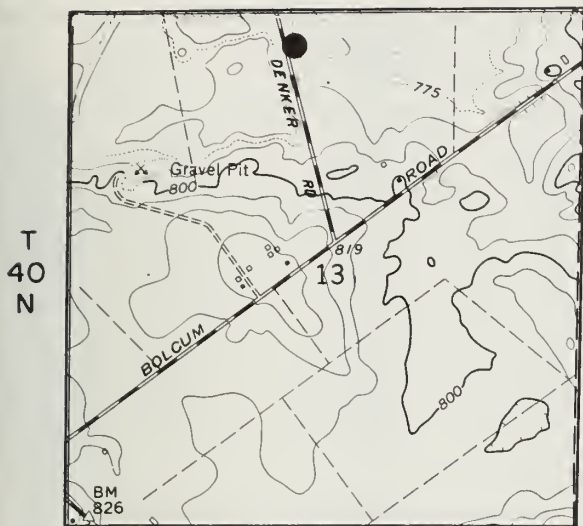
| Sample | Distribution of all parts |                  | Distribution of part < 2.0 mm |                  |           |
|--------|---------------------------|------------------|-------------------------------|------------------|-----------|
|        | > 2.0 mm                  | < 2.0 mm         | .062-<br>2.0 mm               | .004-<br>.062 mm | < .004 mm |
|        | Gravel                    | Sand, silt, clay | Sand                          | Silt             | Clay      |
|        |                           |                  |                               |                  |           |
| 2      | 0                         | 100              | 0                             | 56               | 44        |
| 3      | 6                         | 94               | 24                            | 46               | 30        |
| 4      | 10                        | 90               | 27                            | 40               | 33        |
| 6      | 14                        | 86               | 48                            | 33               | 19        |
| 7      | 4                         | 96               | 26                            | 40               | 34        |
| 8      | 2                         | 98               | 25                            | 41               | 34        |

SIEVE ANALYSES OF ROTARY SAMPLES (in cumulative percent)

| Sample<br>depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|-------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                         | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                         | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| 15.0-20.0               | 0.6                 | 25.5 | 60.6 | 76.4 | 85.9 | 91.8 | 94.7 | 96.0 | 97.0 | 97.5 | 97.8 | 100.0      |

DRILLING RECORD FOR KNE 40N7E-13.5h

R 7 E

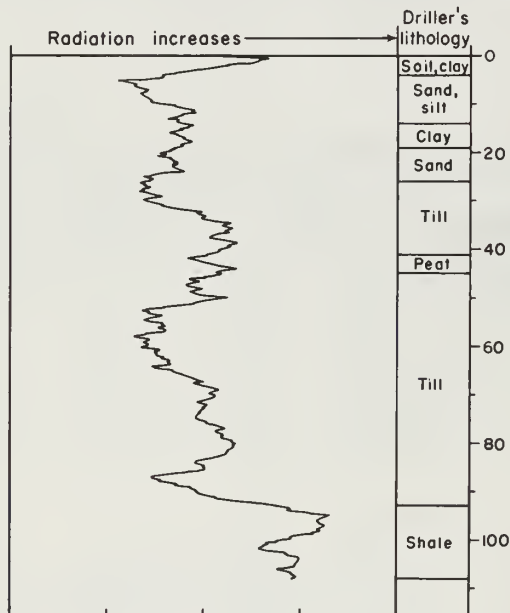


Location of test:

N 5,000 ft, W 3,000 ft from SE  
cor. of sec. 13, S 200 ft  
along Denker Road from a field-  
stone corner post and E 20 ft  
of the center line of Denker  
Road (Elburn Quadrangle, 1964)

Surface elevation: 785 ft  
Date started: 6-2-72  
Date completed: 6-6-72  
Electric log interval: 0-105.0 ft  
Natural gamma log interval: 0-106.0 ft

GAMMA-RAY LOG WITH DRILLER'S LITHOLOGY





KNE 40N7E-13.5h - Continued

DESCRIPTION OF MATERIALS

| Description   | Thickness<br>(ft) | Depth<br>(ft) |
|---|-------------------|---------------|
| Topsoil, black . . . . .  | 0.5               | 0.0 - 0.5     |
| Clay, brown and gray . . . . .  | 3.5               | 0.5 - 4.0     |
| Sand, brown, silty . . . . .  | 5.5               | 4.0 - 9.5     |
| Silt, gray . . . . .  | 4.5               | 9.5 - 14.0    |
| Clay, gray, silty . . . . .   | 5.0               | 14.0 - 19.0   |
| Sand, gray, silty, clay layers . . . . .  | 3.0               | 19.0 - 22.0   |
| Sand and gravel, gray . . . . .   | 4.0               | 22.0 - 26.0   |
| Till, predominantly clay, gray, sandy, gravelly . . .   | 15.0              | 26.0 - 41.0   |
| Peat . . . . .  | 3.5               | 41.0 - 44.5   |
| Till, predominantly clay, gray, sandy, gravelly,<br>boulders . . . . .                            | 25.5              | 44.5 - 70.0   |
| Till, predominantly clay, gray, sandy, gravelly,<br>boulders and sand and gravel layers . . . . . | 23.0              | 70.0 - 93.0   |
| Shale, gray and green . . . . .   | 15.0              | 93.0 - 108.0  |
| Total depth 108.0 ft  |                   |               |

SPLIT-SPOON SAMPLES

| Sample | Depth<br>(ft) | Recovery<br>(in.) | Blows/6-inch<br>hammer drop | N value* | Qp†<br>(tons/ft <sup>2</sup> ) | Moisture<br>content (%) |
|--------|---------------|-------------------|-----------------------------|----------|--------------------------------|-------------------------|
| 1      | 1.0 - 2.5     | 6                 | 2- 4- 5                     | 9        | 1.0                            | 15.5                    |
| 2      | 3.0 - 4.5     | 15                | 4- 6- 9                     | 15       | 3.5                            | 19.3                    |
| 3      | 10.0 - 11.5   | 18                | 4- 5- 4                     | 9        | 1.0                            | 19.8                    |
| 4      | 20.0 - 21.5   | 12                | 12- 15- 13                  | 28       | --                             | --                      |
| 5      | 30.0 - 31.5   | 14                | 3- 6- 6                     | 12       | --                             | 8.64                    |
| 6      | 40.0 - 41.5   | 18                | 12- 17- 23                  | 40       | 4.0                            | --                      |
| 7      | 41.5 - 43.0   | 18                | 11- 26- 47                  | 73       | 3.8                            | --                      |
| 8      | 50.0 - 51.5   | 14                | 11- 15- 23                  | 38       | 4.5+                           | 13.1                    |
| 9      | 60.0 - 61.5   | 15                | 23- 38- 35                  | 73       | 4.5+                           | 7.4                     |
| 10     | 80.0 - 81.5   | 18                | 16- 24- 37                  | 61       | 4.5+                           | 10.2                    |
| 11     | 90.0 - 91.0   | 12                | 37-108 (12-in. total drop)  | 4.5+     | 7.1                            |                         |
| 12     | 95.0 - 96.5   | 18                | 23- 38- 76                  | 114      | 4.5+                           | 14.6                    |

\* Sum of hammer drops in last 12 inches.

† Unconfined compressive strength measurement made with pocket penetrometer.

KNE 40N7E-13.5h - Concluded

SIEVE AND HYDROMETER ANALYSES OF SPLIT-SPOON SAMPLES (in percent)

| Sample         | Distribution of all parts |                  | Distribution of part < 2.0 mm |                  |           |
|----------------|---------------------------|------------------|-------------------------------|------------------|-----------|
|                | > 2.0 mm                  | < 2.0 mm         | .062-<br>2.0 mm               | .004-<br>.062 mm | < .004 mm |
|                | Gravel                    | Sand, silt, clay | Sand                          | Silt             | Clay      |
| 1              | 1                         | 99               | 11                            | 61               | 28        |
| 2              | 0                         | 100              | 8                             | 63               | 29        |
| 3              | 0                         | 100              | 22                            | 61               | 17        |
| 4              | 0                         | 100              | 12                            | 78               | 10        |
| 5              | 11                        | 89               | 47                            | 33               | 20        |
| 6 <sup>1</sup> | 3                         | 97               | 24                            | 40               | 36        |
| 6 <sup>2</sup> | 0                         | 100              | 3                             | 55               | 42        |
| 7 <sup>3</sup> | 1                         | 99               | 15                            | 53               | 32        |
| 8              | 2                         | 98               | 12                            | 49               | 39        |
| 9              | 8                         | 92               | 50                            | 28               | 22        |
| 10             | 7                         | 93               | 25                            | 45               | 30        |
| 11             | 7                         | 93               | 37                            | 35               | 28        |

<sup>1</sup> Interval 40.0 - 40.3 ft.

<sup>2</sup> Interval 40.3 - 41.2 ft.

<sup>3</sup> Interval 41.5 - 41.9 ft.

SIEVE ANALYSES OF SPLIT-SPOON SAMPLES (in cumulative percent)

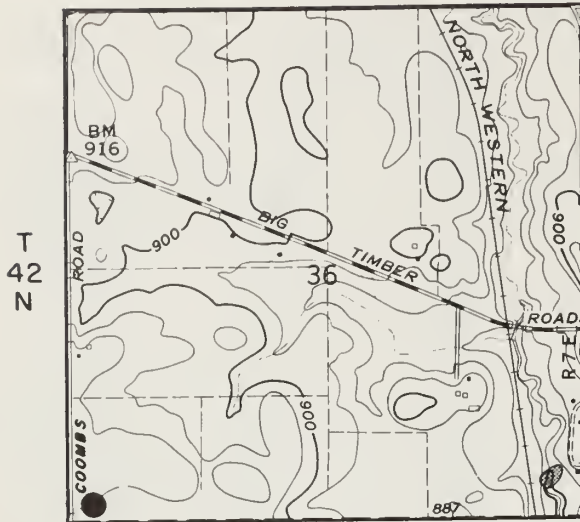
| Sample no.<br>and depth<br>(ft) | Tyler screen number |     |      |     |     |     |     |      |      |      |      |            |
|---------------------------------|---------------------|-----|------|-----|-----|-----|-----|------|------|------|------|------------|
|                                 | 4                   | 9   | 16   | 24  | 32  | 42  | 60  | 80   | 115  | 170  | 250  | Pan        |
|                                 | Gravel              |     | Sand |     |     |     |     |      |      |      |      | Silt, clay |
| <sup>2</sup> 3.0 - 4.5          | 0.0                 | 0.0 | 0.0  | 0.0 | 0.6 | 1.2 | 3.4 | 12.6 | 37.4 | 56.8 | 65.7 | 100.0      |
| <sup>4</sup> 20.0-21.5          | 0.0                 | 0.6 | 1.2  | 1.7 | 2.0 | 2.3 | 4.8 | 13.6 | 37.6 | 55.4 | 60.8 | 100.0      |

SIEVE ANALYSES OF ROTARY SAMPLES (in cumulative percent)

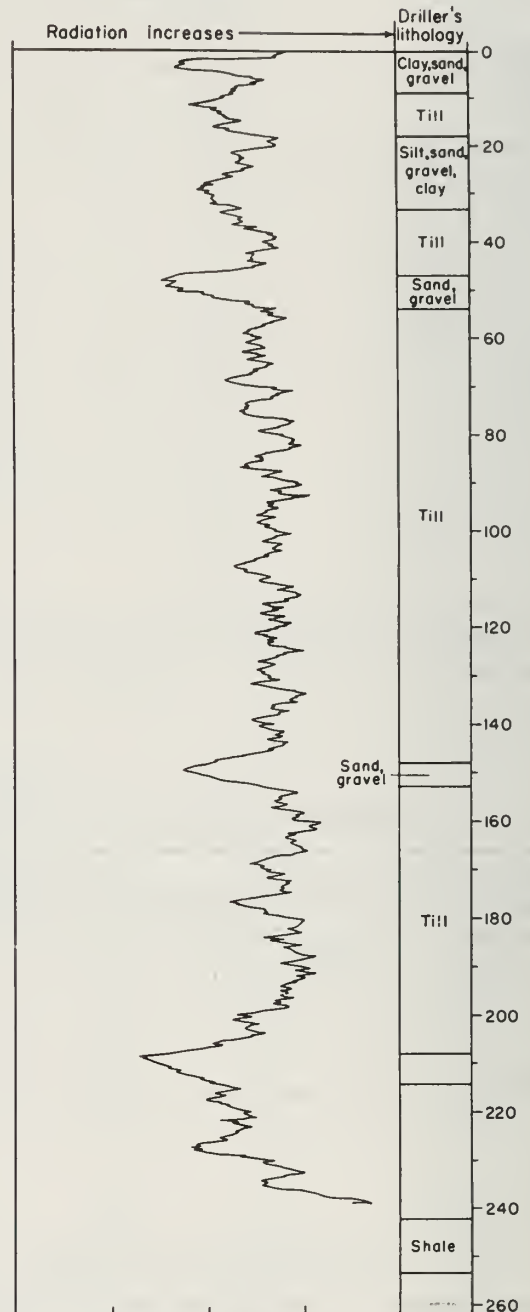
| Sample<br>depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|-------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                         | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                         | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| 20.0-25.0               | 6.6                 | 35.7 | 48.8 | 53.3 | 58.7 | 64.4 | 71.1 | 76.8 | 82.7 | 87.1 | 89.9 | 100.0      |

DRILLING RECORD FOR KNE 42N7E-36.8a

R 7 E



GAMMA-RAY LOG WITH DRILLER'S LITHOLOGY



Location of test:

N 150 ft, E 200 ft from SW cor. of  
sec. 36, N 150 ft and E 200 ft of  
the intersection of the center line  
of Coombs Road east and a lane  
south (Elgin Quadrangle, 1962)

Surface elevation: 920 ft

Date started: 5-19-72

Date completed: 5-24-72

Electric log interval: 0-253.0 ft

Natural gamma log interval: 0-239.0 ft

Zones of fluid loss:

4.0-5.5 ft

Density: 9.6 lb/gal

Viscosity: 43 sec/qt

Loss: 20 gal

47.0-54.0 ft

Density: 9.6 lb/gal

Viscosity: 44 sec/qt

Loss: 30 gal

208.0-214.0 ft

Density: 10.0 lb/gal

Viscosity: 40 sec/qt

Loss: 185 gal

DESCRIPTION OF MATERIALS

| Description  | Thickness<br>(ft) | Depth<br>(ft) |
|--|-------------------|---------------|
| Topsoil, black . . . . .   | 1.5               | 0.0 - 1.5     |
| Clay, brown and gray, sandy . . . . .  | 2.5               | 1.5 - 4.0     |
| Sand and gravel, brown, silty . . . . .  | 1.5               | 4.0 - 5.5     |
| Clay, gray, silty . . . . .  | 3.5               | 5.5 - 9.0     |
| Till, predominantly clay, gray, sandy, sand and<br>gravel layers . . . . .                             | 6.0               | 9.0 - 15.0    |
| Till, predominantly clay, gray, sandy, sand layers . .   | 2.5               | 15.0 - 17.5   |
| Silt, gray, sand layers . . . . .  | 7.0               | 17.5 - 24.5   |
| Sand and gravel . . . . .  | 1.0               | 24.5 - 25.5   |
| Clay, gray, sandy . . . . .  | 4.0               | 25.5 - 29.5   |
| Sand and gravel, gray . . . . .  | 3.5               | 29.5 - 33.0   |
| Till, predominantly clay, gray, sandy, gravelly . . .  | 14.0              | 33.0 - 47.0   |
| Sand and gravel, gray . . . . .  | 7.0               | 47.0 - 54.0   |
| Till, predominantly clay, gray, pink cast, sandy,<br>gravelly . . . . .                                | 16.0              | 54.0 - 70.0   |
| Till, predominantly clay, gray, pink cast, sandy,<br>gravelly, with boulders and sand layers . . . . . | 78.0              | 70.0 - 148.0  |
| Sand and gravel, gray, clayey . . . . .  | 5.5               | 148.0 - 153.5 |
| Till, predominantly clay, gray, sandy, gravelly . . .  | 16.5              | 153.5 - 170.0 |
| Silt, gray, sandy . . . . .  | 4.0               | 170.0 - 174.0 |
| Till, clay, gray, sandy, gravelly . . . . .  | 27.0              | 174.0 - 201.0 |
| Till, predominantly clay, gray, sandy, silty . . . . .   | 7.5               | 201.0 - 208.5 |
| Gravel and boulders, gray and brown . . . . .  | 5.5               | 208.5 - 214.0 |
| Till, predominantly clay, sandy, silty, gravelly,<br>sand and gravel layers, hard . . . . .            | 28.0              | 214.0 - 242.0 |
| Shale, gray . . . . .  | 12.0              | 242.0 - 254.0 |
| Total depth  |                   | 254.0 ft      |

KNE 42N7E-36.8a - Continued

SPLIT-SPOON SAMPLES

| Sample | Depth<br>(ft) | Recovery<br>(in.) | Blows/6-inch<br>hammer drop*   | N value† | Qp‡<br>(tons/ft <sup>2</sup> ) | Moisture<br>content (%) |
|--------|---------------|-------------------|--------------------------------|----------|--------------------------------|-------------------------|
| 1      | 1.0 - 2.5     | 6                 | 3- 4- 5                        | 9        | --                             | --                      |
| 2      | 3.0 - 4.5     | 12                | 2- 5- 9                        | 14       | --                             | 16.7                    |
| 3      | 6.0 - 7.5     | 11                | 3- 5- 7                        | 12       | 2.0                            | 15.5                    |
| 4      | 9.0 - 10.5    | 8                 | 6- 14- 20                      | 34       | --                             | --                      |
| 5      | 12.0 - 13.5   | 13                | 12- 14- 18                     | 32       | 4.5+                           | 13.4                    |
| 6      | 15.0 - 16.5   | 11                | 12- 17- 25                     | 42       | 4.5+                           | 9.1                     |
| 7      | 18.0 - 19.5   | 15                | 13- 17- 16                     | 33       | 4.5+                           | 13.5                    |
| 8      | 21.0 - 22.5   | 16                | 11- 13- 20                     | 33       | 4.5+                           | 11.1                    |
| 9      | 40.0 - 41.5   | 17                | 11- 17- 26                     | 42       | 4.5+                           | 8.5                     |
| 10     | 60.0 - 61.5   | 16                | 11- 20- 29                     | 49       | 3.0                            | 10.3                    |
| 11     | 80.0 - 81.5   | 18                | 11- 23- 31                     | 54       | 2.8                            | 11.1                    |
| 12     | 100.0 - 101.5 | 18                | 13- 16- 26                     | 42       | 1.8                            | 10.7                    |
| 13     | 110.0 - 111.5 | 20                | 16- 19- 31                     | 50       | 3.0                            | 10.6                    |
| 14     | 115.0 - 116.5 | 19                | 11- 19- 23                     | 42       | 2.5                            | 10.4                    |
| 15     | 120.0 - 121.5 | 18                | 12- 19- 21                     | 40       | 2.0                            | 9.5                     |
| 16     | 140.0 - 141.5 | 17                | 13- 26- 45                     | 71       | 4.5+                           | 8.9                     |
| 17     | 160.0 - 161.5 | 15                | 21- 39- 58                     | 97       | 4.5+                           | 9.0                     |
| 18     | 170.0 - 170.5 | 6                 | 120 (6-in. total drop)         | --       | --                             | --                      |
| 19     | 180.0 - 181.5 | 18                | 18- 21- 38                     | 59       | 3.0                            | 10.7                    |
| 20     | 190.0 - 191.5 | 18                | 13- 22- 32                     | 54       | 2.5                            | 13.0                    |
| 21     | 200.0 - 201.5 | 17                | 25- 64-100 (17-in. total drop) | 4.5+     | 9.1                            |                         |
| 22     | 220.0 - 221.5 | 18                | 29- 52- 51 103                 | 4.5+     | 14.4                           |                         |
| 23     | 230.0 - 230.4 | 5                 | 104- 52 (5-in. total drop)     | 4.5+     | 5.3                            |                         |
| 24     | 235.0 - 235.4 | 5                 | 101 (5-in. total drop)         | 4.5+     | 10.1                           |                         |
| 25     | 245.0 - 245.3 | 3                 | 101 (3-in. total drop)         | --       | --                             |                         |

\* Sample 18, sample 23 (last inch), sample 24, and sample 25 - 300 lb hammer.

† Sum of hammer drops in last 12 inches.

‡ Unconfined compressive strength measurement made with a pocket penetrometer.



KNE 42N7E-36.8a - Concluded

SIEVE AND HYDROMETER ANALYSES OF SPLIT-SPOON SAMPLES (in percent)

| Sample | Distribution of all parts |                  | Distribution of part < 2.0 mm |                  |           |
|--------|---------------------------|------------------|-------------------------------|------------------|-----------|
|        | > 2.0 mm                  | < 2.0 mm         | .062-<br>2.0 mm               | .004-<br>.062 mm | < .004 mm |
|        | Gravel                    | Sand, silt, clay | Sand                          | Silt             | Clay      |
|        |                           |                  |                               |                  |           |
| 3      | 0                         | 100              | 1                             | 61               | 38        |
| 4      | 5                         | 95               | 45                            | 44               | 11        |
| 5      | 10                        | 90               | 46                            | 37               | 17        |
| 6      | 9                         | 91               | 40                            | 39               | 21        |
| 7      | 0                         | 100              | 4                             | 61               | 35        |
| 8      | 0                         | 100              | 4                             | 65               | 31        |
| 9      | 7                         | 93               | 30                            | 36               | 34        |
| 10     | 3                         | 97               | 34                            | 33               | 33        |
| 11     | 6                         | 94               | 22                            | 44               | 34        |
| 12     | 3                         | 97               | 27                            | 38               | 35        |
| 13     | 4                         | 96               | 32                            | 32               | 36        |
| 14     | 6                         | 94               | 31                            | 33               | 36        |
| 15     | 5                         | 95               | 31                            | 34               | 35        |
| 16     | 4                         | 96               | 31                            | 37               | 32        |
| 17     | 4                         | 96               | 23                            | 40               | 37        |
| 18     | 0                         | 100              | 53                            | 37               | 10        |
| 19     | 4                         | 96               | 22                            | 37               | 41        |
| 20     | 4                         | 96               | 13                            | 45               | 42        |
| 21     | 7                         | 93               | 32                            | 24               | 44        |
| 22     | 6                         | 94               | 47                            | 31               | 22        |
| 23     | 8                         | 92               | 48                            | 29               | 23        |
| 24     | 22                        | 78               | 31                            | 39               | 30        |

SIEVE ANALYSES OF ROTARY SAMPLES (in cumulative percent)

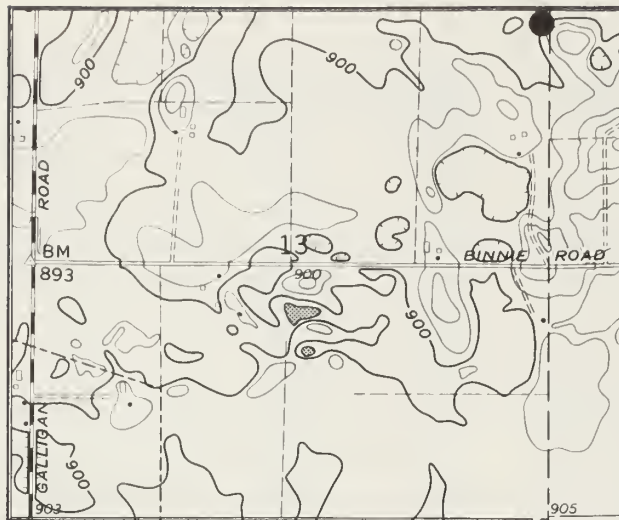
| Sample<br>depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|-------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                         | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                         | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| 50.0- 55.0              | 7.8                 | 55.9 | 77.0 | 82.1 | 86.3 | 89.5 | 93.0 | 94.9 | 96.3 | 97.1 | 97.6 | 100.0      |
| 210.0-215.0             | 12.6                | 39.4 | 59.6 | 65.1 | 70.9 | 76.8 | 84.5 | 89.5 | 93.1 | 95.1 | 96.2 | 100.0      |

DRILLING RECORD FOR KNE 42N7E-13.1h

R 7 E

GAMMA-RAY LOG WITH DRILLER'S LITHOLOGY

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N



Location of test:

N 5,100 ft, W 75 ft from SE cor. of  
sec. 13, S 100 ft and W 75 ft of a  
wooden corner post (Elgin Quadrangle,  
1962)

Surface elevation: 900 ft

Date started: 5-26-72

Date completed: 6-1-72

Casing: 8 in. from surface to 21.0 ft

Electric log interval: 0-242.0 ft

Natural gamma log interval: 0-242.0 ft

Zones of fluid loss:

52.0-74.0 ft

Density: 10.0 lb/gal

Viscosity: 40 sec/qt

Loss: 150 gal

74.0-83.0 ft

Density: 10.0 lb/gal

Viscosity: 40 sec/qt

Loss: 90 gal

204.0-218.0 ft

Density: 10.2 lb/gal

Viscosity: 38 sec/qt

Loss: 150 gal

218.0-224.0 ft

Density: 10.2 lb/gal

Viscosity: 38 sec/qt

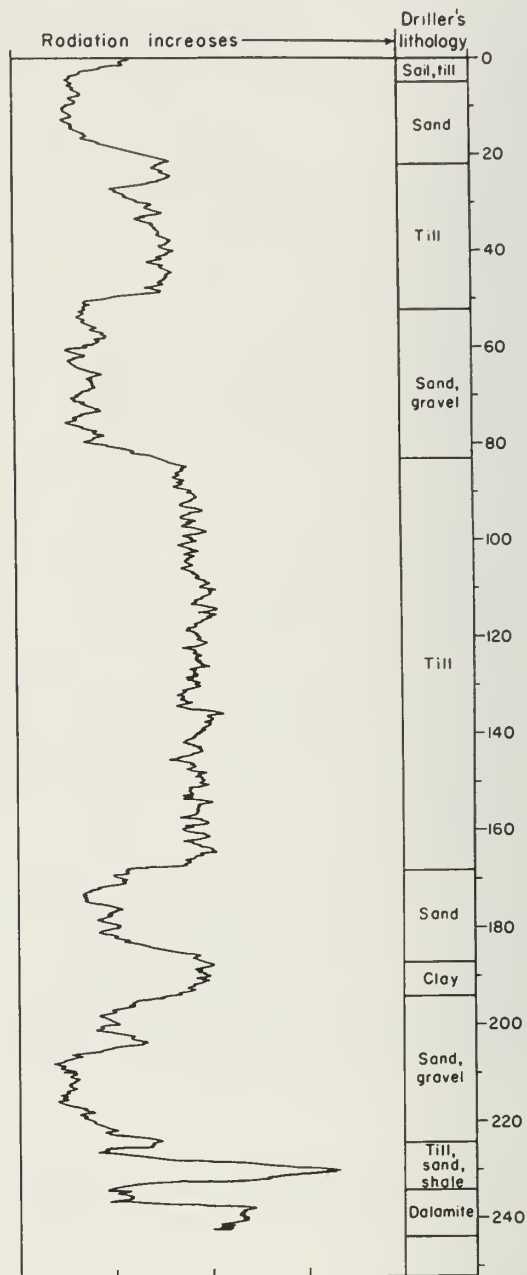
Loss: 45 gal

225.0-229.0 ft

Density: 10.2 lb/gal

Viscosity: 34 sec/qt

Loss: 15 gal



DESCRIPTION OF MATERIALS

| Description  | Thickness<br>(ft) | Depth<br>(ft) |
|--|-------------------|---------------|
| Topsoil, black . . . . .   | 1.0               | 0.0 - 1.0     |
| Till, predominantly clay, gray and brown, sandy,<br>gravelly . . . . .   | 3.5               | 1.0 - 4.5     |
| Sand and gravel, brown, plant remains . . . . .                          | 16.5              | 4.5 - 21.0    |
| Till, predominantly clay, gray, sandy, silty . . . . .                   | 31.0              | 21.0 - 52.0   |
| Sand and gravel, gray, loosely packed . . . . .                          | 22.0              | 52.0 - 74.0   |
| Sand and gravel, gray . . . . .  | 9.0               | 74.0 - 83.0   |
| Till, predominantly clay, gray, pink cast, sandy,<br>gravelly . . . . .  | 64.0              | 83.0 - 147.0  |
| Till, predominantly clay, gray, silty, sandy, gravelly                   | 21.0              | 147.0 - 168.0 |
| Sand, brown . . . . .  | 19.0              | 168.0 - 187.0 |
| Clay, gray, silty, soft . . . . .  | 3.0               | 187.0 - 190.0 |
| Clay, dark gray, silty, trace of wood . . . . .                          | 4.0               | 190.0 - 194.0 |
| Sand, brown, silty, clay layers . . . . .                                | 10.5              | 194.0 - 204.5 |
| Sand and gravel, brown, boulders . . . . .                               | 13.5              | 204.5 - 218.0 |
| Sand and gravel, brown . . . . .   | 6.0               | 218.0 - 224.0 |
| Till, predominantly clay, gray, brown cast, sandy,<br>gravelly . . . . . | 1.5               | 224.0 - 225.5 |
| Sand and gravel, gray, with boulders . . . . .                           | 3.5               | 225.5 - 229.0 |
| Till, predominantly clay, gray, brown cast, sandy,<br>gravelly . . . . . | 3.0               | 229.0 - 232.0 |
| Shale, green and brown . . . . .   | 2.0               | 232.0 - 234.0 |
| Dolomite, gray and shale, green . . . . .                                | 7.0               | 234.0 - 241.0 |
| Dolomite, gray . . . . .   | 3.0               | 241.0 - 244.0 |
| Total depth  |                   | 244.0 ft      |

KNE 42N7E-13.1h - Continued

SPLIT-SPOON SAMPLES

| Sample | Depth<br>(ft) | Recovery<br>(in.) | Blows/6-inch<br>hammer drop | N value* | Qp†<br>(tons/ft <sup>2</sup> ) | Moisture<br>content (%) |
|--------|---------------|-------------------|-----------------------------|----------|--------------------------------|-------------------------|
| 1      | 1.0 - 2.5     | 11                | 1- 2- 3                     | 5        | 1.0                            | 21.5                    |
| 2      | 5.0 - 6.5     | 10                | 9- 11- 14                   | 25       | --                             | --                      |
| 3      | 10.0 - 11.5   | 4                 | 8- 7- 5                     | 12       | --                             | --                      |
| 4      | 15.0 - 16.5   | 14                | 9- 11- 10                   | 21       | --                             | 9.0 <sup>1</sup>        |
| 5      | 20.0 - 21.5   | 13                | 11- 12- 11                  | 23       | 4.0                            | 8.1 <sup>2</sup>        |
| 6      | 30.0 - 31.5   | 16                | 9- 12- 14                   | 26       | 3.5                            | 8.8                     |
| 7      | 50.0 - 51.5   | 18                | 6- 8- 9                     | 17       | 1.0                            | 13.6                    |
| 8      | 70.0 - 71.5   | 5                 | 9- 10- 10                   | 20       | --                             | --                      |
| 9      | 90.0 - 91.5   | 18                | 14- 21- 29                  | 50       | 4.5+                           | 9.5                     |
| 10     | 110.0 - 111.5 | 18                | 15- 29- 39                  | 68       | 4.5+                           | 12.0                    |
| 11     | 130.0 - 131.5 | 18                | 31- 53- 72                  | 125      | 4.5+                           | 11.9                    |
| 12     | 150.0 - 151.5 | 10                | 45- 72-100                  | 172      | 4.5+                           | 9.9                     |
| 13     | 170.0 - 170.5 | 6                 | 154 (6-in. total drop)      | --       | --                             | --                      |
| 14     | 190.0 - 191.5 | 18                | 23- 27- 27                  | 54       | 1.8                            | 20.0                    |
| 15     | 210.0 - 210.9 | 8                 | 63-100 (11-in. total drop)  | --       | --                             | --                      |
| 16     | 230.0 - 230.7 | 7                 | 71-100 (8-in. total drop)   | 4.5+     | 7.8                            |                         |

\*Sum of hammer drops in last 12 inches.

†Unconfined compressive strength measurement made with pocket penetrometer.

<sup>1</sup>Upper 0.8 foot only.

<sup>2</sup>Lower 0.3 foot only.

KNE 42N7E-13.1h - Continued

SIEVE AND HYDROMETER ANALYSES OF SPLIT-SPOON SAMPLES (in percent)

| Sample         | Distribution of all parts |                  | Distribution of part < 2.0 mm |                  |           |
|----------------|---------------------------|------------------|-------------------------------|------------------|-----------|
|                | > 2.0 mm                  | < 2.0 mm         | .062-<br>2.0 mm               | .004-<br>.062 mm | < .004 mm |
|                | Gravel                    | Sand, silt, clay | Sand                          | Silt             | Clay      |
| 1              | 5                         | 95               | 44                            | 31               | 25        |
| 2              | 21                        | 79               | 66                            | 18               | 16        |
| 3              | 19                        | 81               | 77                            | 11               | 12        |
| 4 <sup>1</sup> | 13                        | 87               | 83                            | 8                | 9         |
| 4 <sup>2</sup> | 13                        | 87               | 56                            | 33               | 11        |
| 4 <sup>3</sup> | 11                        | 89               | 79                            | 12               | 9         |
| 5 <sup>4</sup> | 8                         | 92               | 44                            | 45               | 11        |
| 5 <sup>5</sup> | 14                        | 86               | 52                            | 28               | 20        |
| 6              | 10                        | 90               | 36                            | 40               | 24        |
| 7              | 9                         | 91               | 35                            | 36               | 29        |
| 9              | 4                         | 96               | 40                            | 28               | 32        |
| 10             | 4                         | 96               | 33                            | 31               | 36        |
| 11             | 6                         | 94               | 25                            | 40               | 35        |
| 12             | 3                         | 97               | 24                            | 35               | 41        |
| 13             | 0                         | 100              | 65                            | 24               | 11        |
| 14             | 0                         | 100              | 1                             | 24               | 75        |
| 15             | 21                        | 79               | 74                            | 13               | 13        |
| 16             | 1                         | 99               | 39                            | 45               | 16        |

<sup>1</sup>Upper 0.3 ft. <sup>2</sup>Middle 0.25 ft. <sup>3</sup>Lower 0.95 ft. <sup>4</sup>Upper 0.8 ft. <sup>5</sup>Lower 0.3 ft.

SIEVE ANALYSES OF SPLIT-SPOON SAMPLES (in cumulative percent)

| Sample no.<br>and depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|---------------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                                 | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                                 | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| <sup>4</sup> 15.0 - 16.5        | 2.6                 | 22.4 | 33.3 | 39.3 | 45.8 | 56.8 | 69.3 | 78.5 | 86.5 | 91.1 | 92.9 | 100.0      |
| <sup>13</sup> 170.0-170.5       | 0.0                 | 0.7  | 2.1  | 2.9  | 4.1  | 7.9  | 16.2 | 30.0 | 55.3 | 74.3 | 82.5 | 100.0      |
| <sup>15</sup> 210.0-210.9       | 8.8                 | 23.7 | 41.3 | 52.4 | 62.4 | 73.4 | 82.2 | 88.2 | 92.5 | 94.7 | 95.8 | 100.0      |



KNE 42N7E-13.1h - Concluded

SIEVE ANALYSES OF ROTARY SAMPLES (in cumulative percent)

| Sample<br>depth<br>(ft) | Tyler screen number |      |      |      |      |      |      |      |      |      |      |            |
|-------------------------|---------------------|------|------|------|------|------|------|------|------|------|------|------------|
|                         | 4                   | 9    | 16   | 24   | 32   | 42   | 60   | 80   | 115  | 170  | 250  | Pan        |
|                         | Gravel              |      | Sand |      |      |      |      |      |      |      |      | Silt, clay |
| 15.0- 20.0              | 11.4                | 23.5 | 57.7 | 73.5 | 82.6 | 91.1 | 96.3 | 98.5 | 99.4 | 99.6 | 99.7 | 100.0      |
| 60.0- 65.0              | 32.5                | 56.7 | 79.0 | 87.1 | 92.1 | 95.0 | 96.7 | 97.6 | 98.4 | 98.9 | 99.1 | 100.0      |
| 70.0- 75.0              | 9.1                 | 34.6 | 58.7 | 69.5 | 79.4 | 90.6 | 96.4 | 98.2 | 99.1 | 99.4 | 99.6 | 100.0      |
| 170.0-175.0             | 0.0                 | 0.3  | 0.7  | 1.6  | 4.5  | 17.2 | 49.8 | 74.8 | 90.2 | 96.1 | 97.8 | 100.0      |
| 180.0-185.0             | 0.3                 | 0.4  | 0.8  | 1.7  | 3.5  | 10.9 | 41.2 | 71.4 | 90.5 | 97.5 | 99.1 | 100.0      |
| 210.0-215.0             | 15.7                | 56.6 | 76.8 | 81.9 | 85.2 | 88.1 | 91.5 | 93.7 | 95.5 | 96.7 | 97.4 | 100.0      |
| 225.0-230.0             | 22.1                | 43.4 | 55.3 | 60.5 | 66.1 | 74.4 | 84.9 | 90.7 | 94.1 | 95.8 | 96.6 | 100.0      |

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